## Product Highlights

## Low Cost Production Worthy Reference Design

- Only 21 components!
- Single sided board
- Low cost thru-hole components
- Fully assembled and tested
- Easy to evaluate and modify
- Extensive performance data
- Up to $77 \%$ efficiency
- Light weight - no heat sink required for TOPSwitch


## Fully Protected by TOPSwitch

- Primary safety current limit
- Output short circuit protection
- Thermal shutdown protects entire power supply


## Designed for World Wide Operation

- Designed for IEC/UL safety requirements
- Meets VDE Class B EMI specifications


## Typical Applications

- Replacement for low power linear adapters
- Auxiliary power supply for appliance, motor control, utility meters, smart building, UPS, etc.


## Description

The RD2 reference design board is an example of a very low cost production worthy power supply design using the TOPSwitch family of Three-terminal Off-line Switchers from Power Integrations. It is intended to help TOPSwitch users to quickly develop their products by providing a basic design that can be easily modified to fit a particular application. In most cases, a minor change to the transformer for a different output voltage or voltages is all that is needed. A complete set of performance curves, the parts list, the board layout and details on transformer design are provided to speed up the TOPSwitch based switcher design.


Figure 1. RD2 Board Overall Physical Dimensions.

| PARAMETER | LIMITS |
| :--- | :---: |
| Input Voltage Range | 85 to 132 VAC <br> or 170 to 265 VAC |
| Input Frequency Range | 47 to 440 Hz |
| Temperature Range | 0 to $70^{\circ} \mathrm{C}$ |
| Output Voltage ( $\left.\mathrm{I}_{\mathrm{o}}=0.67 \mathrm{~A}\right)$ | $12 \mathrm{~V} \pm 10 \%$ |
| Output Power (continuous) | 8 W |
| Output Power (peak) | 10 W |
| Line Regulation (170-265 VAC) | $\pm 0.7 \%$ |
| Load Regulation (10\%-100\%) | $\pm 5 \%$ |
| Efficiency (115 V input, 8 W out) | $75 \%$ |
| Output Ripple Voltage | $\pm 50 \mathrm{mV} \mathrm{MAX}$ |
| Safety | IEC $950 / \mathrm{UL} 1950$ |
| EMI | VDE B (VFG243 B) <br> CISPR22 |

Figure 2. Table of Key Electrical Parameters.


Figure 3. Schematic Diagram of the RD2 Power Supply.

## CAUTION

The RD2 features a 115/230 VAC selectable input, and is shipped configured for 230 VAC operation (JP1 open). If JP1 is used for 115 VAC operation, it must be removed before applying 230 VAC.


Figure 4. Component Legend of the RD2.

## Component Listing

| Reference | Value | Part Number | Manufacturer |
| :--- | :--- | :--- | :--- |
| U1 |  | TOP210PFI | Power Integrations |
| D1 | $600 \mathrm{~V}, 1 \mathrm{~A}, \mathrm{UFR}$ | UF4005 | General Instruments |
| D2 | Schottky, 3A, 60V | MBR360 | Motorola |
| D3 | 75 V Switching | 1N4148 | Rohm |
| BR1 | $1 \mathrm{~A}, 600 \mathrm{~V}$ | DF06M | General Instruments |
| VR1 | $200 \mathrm{~V} \mathrm{Zener}, \mathrm{1.5} \mathrm{~W}$ | BZY97-C200 | SGS/Thomson, Fagor |
| L1 | $3.3 \mu \mathrm{H}, 4 \mathrm{~A}$ | Custom |  |
| L2 | $8 \mathrm{mH}, 0.2 \mathrm{~A}$ | SU9V-02080 | Tokin |
| C1, C9 | $10 \mu \mathrm{~F}, 200 \mathrm{~V}$ | KMG200VB10RM10X16 | United Chemicon |
| C2 | $330 \mu \mathrm{~F}, 16 \mathrm{~V}$ | LXF16VB331M8X15 | United Chemicon |
| C3 | $120 \mu \mathrm{~F}, 16 \mathrm{~V}$ | LXF16VB121M6.3X11.5 | United Chemicon |
| C5 | $47 \mu \mathrm{~F}, 10 \mathrm{~V}$ | KME10VB47RM5X12.5 | United Chemicon |
| C6 | $47 \mathrm{nF}, 250 \mathrm{VAC}, \mathrm{X} 2$ | F1772-347-2000 | Roederstein |
| C7 | $1 \mathrm{nF}, 250 \mathrm{VAC}, \mathrm{Y} 1$ | DE1110 E 102M ACT4K-KD Murata |  |
| RA, RB | $470 \mathrm{~K}, 1 / 4 \mathrm{~W}$ | 5043CX470K0J | Philips |
| R1 | $6.8 \Omega, 1 / 4 \mathrm{~W}$ | $5043 \mathrm{CX6R800J}$ | Philips |
| R2 | 390 ohms, 1 W | MO-1 391J | Koa/Speer |
| T1 | Custom | T1RD2 |  |
| F1 | $2 \mathrm{~A}, 250 \mathrm{VAC}$ | $19372,2 \mathrm{~A}$ | Wickman |

Figure 5. Parts List for the RD2.

## General Circuit Description

The RD2 is a low-cost, isolated Buck-Boost or flyback switching power supply using the TOP210 integrated circuit. The circuit shown in Figure 3 produces a $12 \mathrm{~V}, 8 \mathrm{~W}$ power supply that operates from 85 to 132 VAC or 170 to 264 VAC input voltage. The 12 V output voltage is determined by the TOPSwitch control pin shunt regulator voltage, the voltage drop of D3, and the turns ratio between the bias and output windings of T 1 . Other output voltages are also possible by adjusting the transformer turns ratios. R1 and C5 provide filtering of the bias winding to improve line and load regulation.

AC power is rectified and filtered by BR1, C 1 and C 9 to create the high voltage DC bus applied to the primary winding of T 1 . The other side of the transformer primary is driven by the integrated high-voltage MOSFET inside the TOP210. JP1 is a jumper used to select 115 V or 230 V operation. Adding JP1 selects 115 V operation. Leaving JP1 open selects 230 V operation. RD2 is supplied with JP1 open. RA and RB equalize leakage currents between C1 and C9. D1 and VR1 clamp the leading-edge voltage spike caused by transformer leakage inductance to a safe value and reduce ringing. The power secondary winding is rectified and filtered by D2, C2, L1, and

C 3 to create the 12 V output voltage. R 2 provides a pre-load on the 12 V output to improve load regulation at light loads. The bias winding is rectified and filtered by D3, R1, and C5 to create a bias voltage to the TOP210. Common-mode EMI currents which flow between the primary windings of the transformer and the secondary output circuitry are attenuated by L2 and C7. Differential-mode EMI currents caused by pulsating currents at the input of the power supply are attenuated by C6 and L2. C5 filters the internal MOSFET gate drive charge current spikes on the Control pin, determines the auto-restart frequency, and together with R1, compensates the control loop.

The circuit performance data shown in Figures 6-18 was measured with AC voltage applied to the RD2.

Load Regulation (Figure 6) - The amount of change in the DC output voltage for a given change in output current is referred to as load regulation. The 12 V output stays within $\pm 5 \%$ from $10 \%$ to $100 \%$ of rated load current. The TOPSwitch on-chip overtemperature protection circuit will safely shut down the power supply under sustained overload conditions.

## General Circuit Description (cont.)

Line Regulation (Figure 7) - The amount of change in the DC output voltage for a given change in the AC input voltage is called line regulation. The maximum change in output voltage is less than $\pm 0.7 \%$.

Efficiency (Line Dependent) - Efficiency is the ratio of the output power to the input power. The curves in Figures 8 and 9 show how the efficiency changes with input voltage. Curves are also given to show the difference in efficiency when C 1 and C 9 are changed from $10 \mu \mathrm{~F}$ to $22 \mu \mathrm{~F}$.

Efficiency (Load Dependent) - The curves in Figures 10 and 11 show how the efficiency changes with output power at 115 and 230 VAC inputs. The curves also show the increase in efficiency when C 1 and C 9 are changed from $10 \mu \mathrm{~F}$ to $22 \mu \mathrm{~F}$.

Power Supply Turn On Sequence - The internal switched, highvoltage current source provides the initial bias current for TOPSwitch when power is first applied. The waveforms shown in Figure 12 illustrate the relationship between the high-voltage

DC bus and 12 V output voltage. Capacitors C 1 and C 9 charge to the peak of the AC input voltage before TOPSwitch turns on. The delay of 150 ms (typical) is caused by the time required to charge the auto-restart capacitor C 5 to 5.7 V . At this point the power supply turns on as shown.

Figure 13 shows the output voltage turn on transient.
Line frequency ripple voltage is shown in Figure 14 for 115 VAC input and 8 W output. Switching frequency ripple voltage is shown in Figure 15 for the same test condition.

The power supply transient response to a step load change from 0.5 A to 0.67 A ( $75 \%$ to $100 \%$ ) is shown in Figure 16. Note that the response is quick and well damped.

The RD2 is designed to meet worldwide safety and EMI (VDE B) specifications. Measured conducted emissions are shown in Figure 17 for 115 VAC and Figure 18 for 230 VAC.


Figure 7. Line Regulation


Figure 8. Efficiency vs. Input Voltage, 85-132 VAC


Figure 10. Efficiency vs. Output Power, 115 VAC Input


Figure 12. Turn On Delay


Figure 9. Efficiency vs. Input Voltage, 170-265 VAC


Figure 11. Efficiency vs. Output Power, 230 VAC Input


Figure 13. Output Voltage Turn On Transient


Figure 14. Line Frequency Ripple, 115VAC In, $8 W$ Output


Figure 15. Switching Frequency Ripple, 115 VAC In, 8W Output


Figure 16. Transient Load Response (75\% to $100 \%$ of load)


Figure 17. EMI Characteristics at 115 VAC Input.


Figure 18. EMI Characteristics at 230 VAC Input.


CORE\# - PC40 EE16 (TDK) GAP FOR AL OF $250 \mathrm{nH} / \mathrm{T}^{2}$ BOBBIN\# - BE-16-118CPH (TDK)


| ELECTRICAL SPECIFICATIONS |  |  |  |
| :---: | :---: | :---: | :---: |
| Electrical Strength | $60 \mathrm{~Hz}, 1$ minute, <br> from pins $1-4$ to pins 5, 8 <br> Creepage <br> Between pins 1-4 and pins 5, 8 | 3000 VAC |  |
| Primary Inductance | All windings open | 4.0 mm (min) |  |
| Resonant Frequency | All windings open | $700 \mathrm{kHz}(\mathrm{min})$ |  |
| Primary Leakage Inductance | Pins 5 and 8 shorted | $50 \mu \mathrm{H}$ (max) |  |

NOTE: All inductance measurements should be made at 100 kHz

Figure 19. Electrical specification of transformer T1RD2


| WINDING INSTRUCTIONS |  |
| :---: | :--- |
| Two-layer "C" Wound Primary | Start at pin 2. Wind 65 turns of 38 AWG heavy nyleze <br> wire from left to right. Apply 1 layer of tape (white <br> polyester film 8.3 mm (0.32 in.) wide by 0.056 mm <br> (2.2 mil) thick) for basic insulation. Continue winding <br> 65 turns from right to left. Finish at pin1. |
| Basic Insulation | Apply 2 layers of tape for basic insulation. <br> Start at pin 8. Wind12 turns of triple-insulated <br> 26 AWG wire* from right to left. <br> Finish at pin 5. |
| Triple Insulated Secondary |  |
| Apply 2 layers of tape for basic insulation. |  |
| Barallel Bifilar Primary Bias | Start at pin 4. Wind 6 turns of 28 AWG triple insulated <br> wire* parallel bifilar in a single layer, from left to right. <br> Finish at pin 3. <br> Apply 3 layers of tape for basic insulation. |
| Final Assembly Insulation | Assemble and secure core halves. <br> Impregnate uniformly with varnish. |

* Triple insulated wire sources.

| $\mathrm{P} / \mathrm{N}$ : order by description | P/N: order by description | iption |  |
| :---: | :---: | :---: | :---: |
| Rubudue Wire Company | Furukawa Electric America, Inc. | The Furukawa Electric Co., Ltd |  |
| 5150 E. La Palma Avenue | 200 Westpark Drive | 6-1, Marunouchi 2-chome, |  |
| Suite 108 | Suite 190 | Chiyoda-ku, Tokyo 100, Japan |  |
| Anaheim Hills, CA 92807 | Peachtree City, GA 30269 | 81-3-3286-3226 |  |
| (714) 693-5512 | (770) 487-1234 | 81-3-3286-3747 FAX |  |
| (714) 693-5515 FAX | (770) 487-9910 FAX |  | Pr-1740-01059 |

Figure 20. Construction details of transformer T1RD2

Notes

Notes

Notes

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